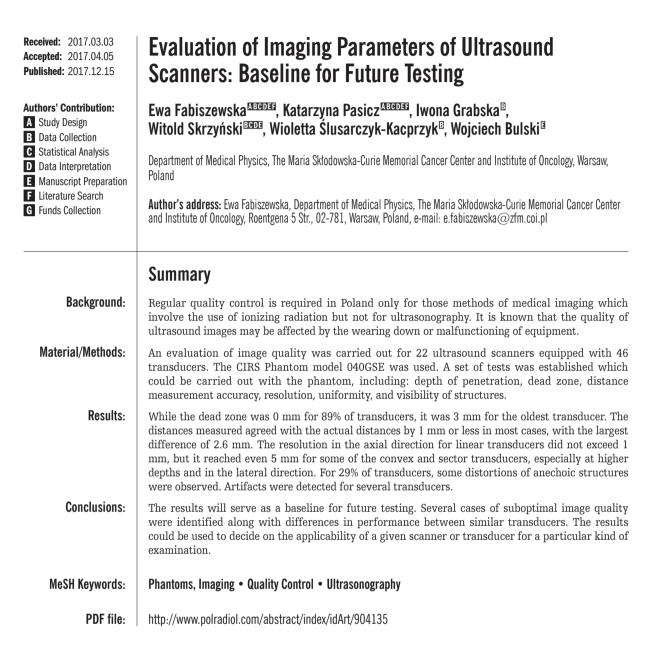


Polish

Journal of Rad

**ORIGINAL ARTICLE** 



# **Background**

Ultrasonography is currently one of the most widely used methods of medical imaging of soft tissues, the circulatory system, and the nervous system, with new applications being constantly developed [1-6]. One of the main advantages of ultrasonography is the lack of ionizing radiation and the risks associated with it. With spatial resolution reaching 0.5 mm, ultrasonography can provide a good quality of images. However, as shown in many publications [7-16], the quality should be systematically controlled. For example, Mårtensson et al. have shown that 40% of 676 ultrasound transducers used in 32 hospitals in southern Sweden were defective [7]. In the results published by

Sipilä et al. [8], 25% of the transducers evaluated had physical flaws, and for 15% of the transducers image guality was defective.

Regular quality control is required by law in Poland for those methods of medical imaging which involve the use of ionizing radiation [17,18]. Despite a rising number of ultrasound scanners and examinations, systematic quality control of ultrasound equipment is not required.

In the present study, imaging parameters of ultrasound equipment were evaluated for ultrasound scanners and transducers used in the Maria Skłodowska-Curie Memorial Cancer Center and Institute of Oncology in Warsaw, Poland (COI).

Test methods and acceptance criteria were based on APPM and IPEM reports and on the Gammex/RMI manual [9,10,16].

## **Material and Methods**

### Ultrasonography equipment

Evaluation of image quality was carried out between November 2015 and March 2016 for 22 ultrasound scanners equipped with 46 transducers (22 linear, 19 convex, 5 sector transducers), comprising 92% of all the scanners in the COI. All tests were performed for B-mode presentation images. A list of all the tested ultrasound scanners is presented in Table 1.

### **Ultrasound frequency range**

All transducers were broad-band, with frequencies in the range of 4–18 MHz for linear transducers, 1–6 MHz for convex transducers, and 1-5 MHz for sector transducers. For some ultrasound scanners, it was possible to choose one of three frequency ranges, namely "Res", "Gen", and "Pen". "Res" stands for "resolution" and refers to the highest frequency range; this mode is meant for imaging superficial tissues (optimization of resolution is done at the cost of the range). "Pen" stands for "penetration" and refers to the lowest frequencies; it is meant for deeply located tissues or patients with obesity. "Gen", which is usually the default setting, stands for "general" and designates an intermediate range of frequencies [19].

#### Equipment

A Multi-Purpose, Multi-Tissue Ultrasound Phantom model 040GSE manufactured by CIRS (Computerized Imaging Reference Systems Inc.) [20] was used to test the ultrasound scanners. The phantom is filled with a gel material called Zerdine® (a trade name). The speed of ultrasound in the material is 1540±10 m/s. The phantom is divided into two parts with different attenuation coefficients to mimic different tissues; namely, 0.5 dB/(cm·MHz) and 0.7 dB/(cm·MHz). The phantom contains several sets of objects for the evaluation of the dead zone, the axial and lateral resolution, the visibility of structures with various contrast (grayscale), and the visibility of anechoic structures. Additionally, several small targets are placed at known distances in horizontal and vertical directions for verification of distance measurement accuracy. A scheme of the phantom is presented in Figure 1.

#### Conditions for the assessment of image quality

Results of the evaluation of image quality strongly depend on scanner settings, such as the anatomical program, gain, harmonic mode etc. [21]. The following conditions were met during the measurements:

- The same anatomical program (preset) as used clinically (based on user information);
- TCG (time gain compensation) optimized for good uniformity of the image;
- Focal zone on the evaluated structure;
- Depth optimized for the best visibility of the evaluated structure.

Table 1. List of evaluated ultrasound scanners and transducers.

Manufacturer	Туре	Year of manufacture	
Siemens	Acuson S2000	2013	
	ACUSON Aspen	2002	
	HDI 5000 SonoCT	2005	
-	IU22	2010	
	Sparq	2013	
Philips	IU22	2007	
	HD15	2014	
-	HDI 4000	2003	
-	HD 15 Pure Wave	2014	
	HI Vision Preirus	2014	
-	Prosound Alpha 7	2011	
-	HI Vision Preirus	2014	
Hitachi	HI Vision Preirus	2015	
-	HI Vision 900	2007	
-	HI Vision 900	2007	
-	EUB 7500	2008	
471	Ultra Mark 4 Plus	1995	
ATL -	HDI 3000	1997	
GE Healthcare	Voluson 730 EXP	2002	
OLYMPUS	EU-ME2	2015	
Supersonic Imagine	AIXPLORE	2012	
BK Medical	Ultra View 800 Pro Focus	2012	

Advanced functions, such as harmonic mode, Sono CT, XRes and similar, were turned off. All the settings were noted down for reference during future tests. Displayed values of MI and TI or TIB indexes were also recorded for comparison in future tests.

#### Scope of tests and criteria

For each scanner and each transducer, the following parameters were evaluated visually:

- Depth of penetration;
- Dead zone;
- Distance measurement accuracy in horizontal and vertical directions;
- Axial and lateral resolution;
- Uniformity;
- · Visibility of anechoic structures;
- Visibility of structures with various contrast (grayscale).

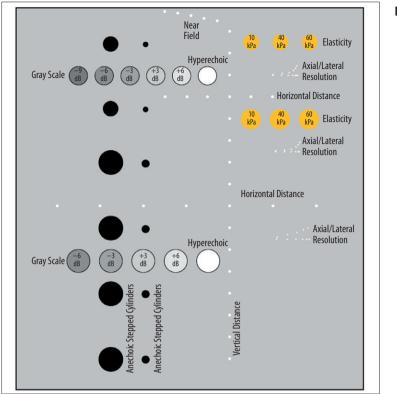


Figure 1. Scheme of the phantom used for evaluation of ultrasound scanners (source: [20]). During measurements, the transducer is in contact with the top surface of the phantom.

The scope of the tests was based on APPM and IPEM reports and on the Gammex/RMI manual [9,10,16]. We chose such tests that could be carried out with the CIRS 040GSE phantom in the same way for as many scanners and transducers as possible. Apart from the distance measurement accuracy, all the tests were based purely on visual assessment of images. Visual evaluation of image quality was carried out by the same observers for all ultrasound scanners in order to eliminate inter-observer variability. All of the tests were done separately for two areas with different attenuation coefficients (0.5 dB/(cm·MHz) and 0.7 dB/(cm·MHz)).

Depth of penetration was defined as the maximum depth at which the background texture of the image was still distinguishable from electronic noise. The depth of penetration depends on ultrasound frequency, output power of the transducer, gain and TGC settings, focal depth, the display format (number of lines), and electronic noise. It can change in such cases as output intensity alternations or due to a physical damage of the transducer or cable.

The dead zone is the distance between the front surface of the transducer and the echo of the first visible "near field" structure (Figure 1). The existence of the dead zone is caused, among other reasons, by the finite length of each emitted pulse. Echoes from low depths may be not detected if they coincide in time with the excitation pulse. If the frequency of pulses is higher, the pulses are shorter and the dead zone is smaller. The dead zone can get larger if the pulses are longer, which can be caused, for example, by a crack in the piezoelectric crystal or a malfunction of electronics.

The accuracy of distance measurement was evaluated by comparing known distances between the phantom structures with the distances measured with the software of the ultrasound scanners. The distances were measured between the structures identified in Figure 1 as the "horizontal distance" and the "vertical distance" (in two perpendicular directions). Ultrasound scanners measure the time between pulse emission and echo registration, and convert the measured time into a distance with the assumption that the speed of ultrasound in tissues is constant. Distance errors can be caused by a failure of the internal clock of the scanner. An error of the horizontal distance can be also caused by a failure of the scan mechanism. This is possible especially in mechanical transducers in which the wear of the motor can affect the timing of the acquisition of each line of the B-mode presentation image. Obviously, the distances measured will be erroneous if the speed of ultrasound in the phantom material is different than the speed assumed in the tissue. It is worth noting that the speed of ultrasound in phantoms usually depends on temperature (a change of approximately 1.5 m/s per 1°C).

The resolution in axial and lateral directions was evaluated visually by identifying the nearest objects which could be clearly identified as separate and by recording the distance between the objects. The resolution in the axial direction (along the axis of the ultrasound beam) is limited by the wavelength and by the length of the ultrasound pulse. The resolution in the lateral direction (along the line perpendicular to the ultrasound beam) is approximately equal to the width of the ultrasound beam, and changes when the depth, focal zone, gain, or sensitivity settings are changed. When possible, resolution in both directions was evaluated at three different depths (3.0 cm, 6.5 cm and 10.0 cm). For systems with multiple focal zones or with dynamic focus, the resolution in the lateral direction is uniform over a

Score	Shape	Edge	Interior
1	Round	Sharp	Black (anechoic)
2	Elliptical	Blurred	Single bright pixels
3	>20% difference between width and height	Hard to define	Filled with bright pixels

Table 2. Score scale for visibility of anechoic structures.

Table 3. Criteria for evaluation of test results.

Test	Suggested action level	Suggested defect level	
Depth of penetration	Change from baseline $\geq$ 0,6 cm	Change from baseline $\geq$ 1.0 cm	
Dead zone	7 mm for f <3 MHz 5 mm for 3 MHz< f <7 MHz 3 mm for f ≥7 MHz	10 mm for f <3 MHz 7 mm for 3 MHz< f <7 MHz 4 mm for f ≥7 MHz	
Distance accuracy - vertical	≥1.5 mm or 1.5%	$\geq$ 2 mm or 2%	
Distance accuracy – horizontal	≥2% or 2 mm	$\geq$ 3% or 3 mm	
Axial resolution	Change from baseline	Change from baseline	
Lateral resolution	Change from baseline	Change from baseline	
Uniformity	formity Change from baseline Change f		
Visibility of anechoic structures	c structures Change from baseline Change from baseline		
Visibility of structures with various contrast (grayscale)	Change from baseline	Change from baseline	

larger range of depths. The resolution in the lateral direction can be affected by malfunction of elements of transducers or of the beam-forming system.

Image uniformity, which is an essential parameter of image quality, was evaluated visually by the observation of uniform regions of the phantom. The presence of non-uniformities and artifacts may mask real structures or may lead to diagnosis of non-existent pathologies.

Visibility of anechoic structures depends on spatial resolution, contrast resolution, uniformity, and the presence of electronic noise and side lobes of the beam. Three parameters describing visibility of anechoic structures were used: their shape (it should be round), the edges (sharpness), and the interior (it should be anechoic). Each of those three parameters was scored on a three-step scale (details in Table 2). Overall, a total score of 3 referred to the best image, and 9 was the worst possible score. The visibility of structures with various contrast (–9 dB, –6 dB, –3 dB, +3 dB, +6 dB, >15 dB) was scored with one point for each visible structure.

The results were compared with the criteria outlined in Table 3, based on APPM and IPEM reports and on the Gammex/RMI manual [9,10,16]. Two levels of criteria are defined. If the results exceed action levels, a corrective action should be taken to ensure that the results will not exceed defect levels. For some tests, including the depth of penetration and the visibility of structures, the results are compared with baseline values (results obtained during the first tests, usually after the installation of the scanner).

## Results

Table 4 and Figure 2 present the depth of penetration for the transducers evaluated. As there were no baseline values, it was not possible to decide on the acceptance of the results. During the analysis of the results, it was noted that for one convex transducer the results were obviously different than for the rest of them. The depth of penetration for that particular transducer was 5.4 cm for a 0.5 dB/ (cm·MHz) attenuation, which would be a rather typical result for a linear transducer.

The dead zone test results are presented in Figure 3. The results were acceptable, none of the values exceeded the levels presented in Table 3. For 89% of the transducers controlled, the dead zone was 0 mm. The largest and worst result (3 mm) was obtained for one sector transducer. Interestingly, it was the oldest one, in use since 1995.

Table 5 and Figures 4 and 5 present results of the distance accuracy test. None of the results exceeded the levels presented in Table 3. Maximum errors of the measured distance were observed for one of the convex transducers and were 2 mm in the vertical direction and 2.6 mm in the horizontal direction.

#### Attenuation 0.5 dB/(cm·MHz) Attenuation 0.7 dB/(cm·MHz) Minimum [cm] Maximum [cm] Median [cm] Minimum [cm] Maximum [cm] Median [cm] 5.0 5.5 Linear 3.0 8.0 3.1 4.0 Transducer 5.4 17.0 12.2 5.5 12.0 9.6 Convex type Sector 12.3 16.0 13.0 9.0 13.0 10.6 20 20 20 Linear Convex Sector Attenuation 0.5 dB/ (cm×MHz) Number of transducers 10 10 10 0 0 0 5 10 15 20 5 10 15 20 15 0 5 10 20 0 0 20 20 20 Attenuation 0.7 dB/ (cm×MHz) Number of transducers 10 10 10 0 0 0 5 10 15 20 0 10 15 20 10 20 0 5 0 5 15 Depth of penetration [cm] Depth of penetration [cm] Depth of penetration [cm]

#### Table 4. Results of the depth of penetration test.

Figure 2. Results of the depth of penetration test.

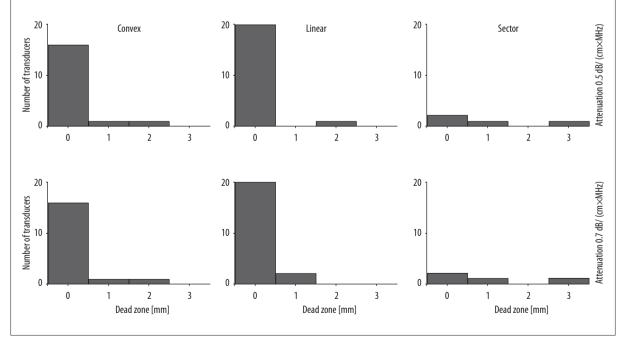




Table 5. Results of the test of distance accuracy in two directions.

			Maximum difference between nominal and measure distance [mm]			
		Attenuation 0.5 dB/(o	cm∙MHz)	Attenuation 0.7 dB/(cm·MHz)		
Horizontal direction						
	Linear		1.7		1.1	
Transducer type	Convex		2.6		2.0	
	Sector		1.6		1.5	
/ertical Direction						
	Linear		1.2		1.7	
Transducer type	Convex		2.0		2.0	
	Sector		1.0		1.4	
Number of transducers	Convex 2	20 10 3 0	Linear 1 2		Sector 1 2	3
20 January		20		20		(-HW)

Figure 4. Difference between nominal and measured distance in the horizontal direction.

10

٥

3

0

1

Table 6 presents the results of the axial resolution test. The resolution for linear transducers was at least 1 mm. It was worse for convex transducers, especially at higher depths, but did not exceed 5 mm.

2

Horizontal distance error [mm]

Table 7 presents the results of the lateral resolution test. The resolution did not exceed 5 mm, and the best results were obtained for linear transducers (between 0.5 mm and 3 mm). Similar to the axial direction, the results were worse at higher depths. The results of the resolution test will serve as a baseline for future testing.

As a result of the uniformity test, line artifacts were detected for three linear and one convex transducer. The images were very noisy for three linear and one convex transducer. For two linear transducers, it was not possible to regulate the gain. The visibility of anechoic structures is presented in Figure 6. For 71% of transducers, there were no distortions of shape, edges, or of the interior of structures, and the total score was 3. However, for the rest of the transducers, suboptimal image quality was observed, and the score was between 4 and 8 points. The largest distortion of anechoic structures was observed for one convex transducer (8 points).

1

10

0

0

3

2

Horizontal distance error [mm]

Attenuation 0.7 dB/

3

2

Horizontal distance error [mm]

Figure 7 presents the number of distinguishable structures with different contrasts (grayscale). For 89% of transducers, 5 or more structures were visible. For four transducers, only 4 structures were visible, and for one linear transducer only 2 structures were visible in the higher attenuation zone.

Number of tran:

10

0

0

1

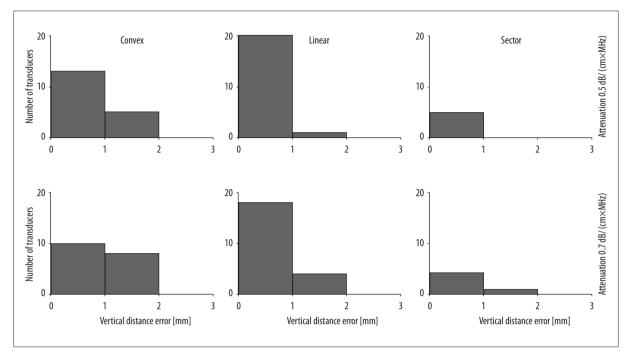


Figure 5. Difference between nominal and measured distance in the vertical direction.

Table 6. Resolution in the axial direction.

			Resolution in axial direction [mm]				
		Attenuation 0.	Attenuation 0.5 dB/(cm·MHz)		.7 dB/(cm·MHz)		
		Minimum	Maximum	Minimum	Maximum		
Location of resolution	n pattern (depth): 3.0	m					
	Linear	0.25	1.0	0.25	1.0		
Transducer type	Convex	1.0	2.0	0.25	1.0		
	Sector	0.5	4.0	0.5	2.0		
Location of resolution	n pattern (depth): 6.5 o	m					
	Linear	0.5	1.0	1.0	Х		
Transducer type	Convex	0.5	4.0	1.0	2.0		
	Sector	0.5	4.0	1.0	4.0		
Location of resolutio	n pattern (depth): 10.5	cm					
Transducer type	Linear	Х	Х	Х	Х		
	Convex	1.0	4.0	1.0	5.0		
	Sector	2.0	4.0	2.0	х		

## Discussion

The AAPM report on quality control procedures in ultrasonography [9] and other similar documents outline the methods for testing of quality. For some tests, such as distance measurement, the documents give clear acceptance criteria. It is then possible to evaluate the results, even if the test is carried out for the first time. For some tests, such as the depth of visualization, absolute criteria are not available. The results of initial tests become a baseline against which the results of subsequent tests are compared. It is easy to say if the results are constant but not if they are optimal. At the same time, the depth of visualization is very important clinically. Serious differences were observed in the present study between the results for similar transducers. The depth of visualization for linear transducers ranged from 3 cm to 8 cm. It seems that not all of these transducers can be used in examinations of the same anatomical regions, despite that they are all linear. The same applies to convex transducers, with the depth of penetration ranging from 5.4 cm to 17 cm.

## Table 7. Resolution in the lateral direction.

		Resolution in lateral direction [mm]				
	_	Attenuation 0.5 dB/(cm·MHz)		Attenuation 0.	7 dB/(cm∙MHz)	
		Minimum	Maximum	Minimum	Maximum	
Location of resolution	on pattern (depth): 3.0 cm					
	Linear	0.5	3.0	0.5	3.0	
Transducer type	Convex	0.5	4.0	2.0	3.0	
	Sector	1.0	4.0	2.0	3.0	
ocation of resolutio	on pattern (depth): 6.5 cm					
	Linear	1.0	2.0	2.0	Х	
ransducer type	Convex	1.0	4.0	2.0	4.0	
	Sector	2.0	4.0	3.0	4.0	
ocation of resolutio	on pattern (depth): 10.5 cm					
	Linear	Х	Х	Х	Х	
Transducer type	Convex	2.0	5.0	2.0	5.0	
	Sector	4.0	5.0	4.0	5.0	
20 Light contractions of the second s	Convex		Linear 5 6 7 8	20 Secto 10	r 6 7 8	
20 0 Lausancers 0 L		20 1		20 10		
0	5 6 7 8 Anechoic structures score	0	5 6 7 8 echoic structures score	03 4 5 Anechoic s	6 7 8 tructures score	

Figure 6. Visibility of anechoic structures. A score of 3 points means no distortions, a higher score represents suboptimal image quality.

The tests described in the present study may be used to evaluate imaging parameters of ultrasound scanners. If the tests are repeated periodically, a decrease in parameters may be detected due to the wearing down or damage of the equipment. The test results could be used to decide on the applicability of the scanner and transducer for a given kind of examination. Polish standards of ultrasound examinations [1] outline technical requirements for equipment used in various types of examinations. For instance, examinations of the thyroid should be performed with a linear transducer which should be broad-band (5–10 MHz), have a minimum of 128 channels, etc. The standards do not specify direct requirements for the depth of visualization or the resolution. The decision on the applicability of the transducer has then to be based on the knowledge and experience of physicians and ultrasonographers.

A few other transducers were also tested, e.g. endoscopic ones. However, the phantom was not designed for such transducers, and usually it was not possible to carry out a

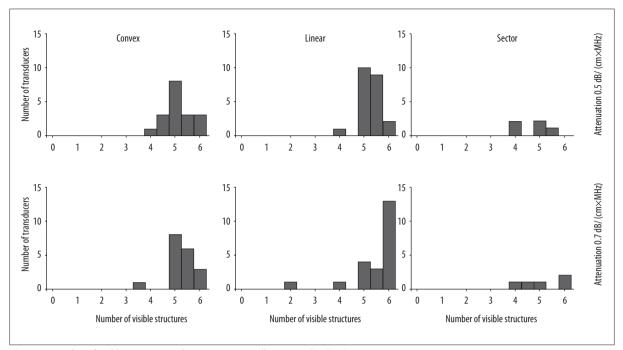


Figure 7. Number of visible structures with various contrasts (largest result is best).

full set of tests. Therefore, only the results for linear, convex, and sector transducers are presented.

The tests described herein were based on visual assessment of the images. A maximum of care has been taken to perform the tests for all scanners in a reproducible manner. Nevertheless, objectivity and reproducibility of the results could have been be improved, if numerical methods of image analysis had been used. It is generally possible to evaluate several parameters in an objective way [14,22,23], but the possibility of export of captured images is required. Unfortunately, for most of the ultrasound scanners evaluated in the present study, DICOM export was not possible, and the possibility of export in other formats was varied.

#### **References**:

- Jakubowski W (ed.): Ultrasound examinations standards of the Polish Ultrasound Society. 4<sup>th</sup> ed. Warszawa: Roztoczańska Szkoła Ultrasonografii, 2011 [in Polish]
- Nowicki A: Ultrasound in medicine introduction to modern ultrasonography. Warszawa: Roztoczańska Szkoła Ultrasonografii, 2010 [in Polish]
- Staryszak J, Stopa J, Kucharska Miąsik I et al: Usefulness of ultrasound examinations in the diagnostics of necrotizing enterocolitis. Pol J Radiol, 2015; 80: 1–9
- 4. Wawrzyk M, Sokal J, Andrzejewska E, Przewratil P: The role of ultrasound imaging of callus formation in the treatment of long bone fractures in children. Pol J Radiol, 2015; 80: 473–78
- Paluch Ł, Nawrocka-Laskus E, Wieczorek J et al: Use of ultrasound elastography in the assessment of the musculoskeletal system. Pol J Radiol, 2016; 81: 240–46
- Bombiński P, Warchoł S, Brzewski M et al: Ultrasonography of extravaginal testicular torsion in neonates. Pol J Radiol, 2016; 81: 469–72
- Mårtensson M, Olsson M, Segall B et al: High incidence of defective ultrasound transducers in use in routine clinical practice. Eur J Echocardiogr, 2009; 10(3): 389–94
- Sipilä O, Mannila V, Vartiainen E: Ouality assurance in diagnostic ultrasound. EurJ Radiol, 2011; 80(2): 519–25

## Conclusions

Tests of imaging parameters of ultrasound scanners have been carried out for the first time in the Maria Skłodowska-Curie Memorial Cancer Center and Institute of Oncology. The results will serve as baseline for future testing. Several cases of suboptimal image quality were identified along with differences in performances between similar transducers. The results could be used to decide on the applicability of a given scanner and transducer for a particular kind of examination.

- 9. Goodsitt MM, Carson P, Witt S et al: Real-time B-mode ultrasound quality control test procedures. Report of AAPM Ultrasound Task Group No. 1. Med Phys, 1998; 25(8): 1385–406
- Russell S, Dudley N, Evans T et al: Quality assurance of ultrasound imaging systems. IPEM Report No. 102. York: IPEM, 2010
- Thjissen JM, van Wijk MC, Cuypers MH: Performance testing of medical echo/Doppler equipment. Eur J Ultrasound, 2002; 15(3): 151-64
- Hangiandreou NJ, Stekel SF, Tradup DJ et al: Four-year experience with a clinical ultrasound quality control program. Ultrasound Med Biol, 2011; 37(8): 1350–57
- Mårtensson M, Olsson M, Brodin LÅ: Ultrasound transducer function: Annual testing is not sufficient. Eur J Echocardiogr, 2010; 11(9): 801–5
- Browne E, Watson AJ, Gibson NM et al: Objective measurements of image quality. Ultrasound Med Biol, 2004; 30(2): 229–37
- Dudley NJ, Griffith K, Houldsworth G et al: A review of two alternative ultrasound quality assurance programmes. Eur J Ultrasound, 2001; 12(3): 233–45
- Gammex/RMI. The QC Cookbook for Ultrasound. Middleton, WI: Gammex/RMI, 1994

- Regulation of Polish Minister of Health of 12 November 2015 on safe use of ionizing radiation for medical exposures. Polish Journal of Laws from 2015, item 2040 [in Polish]
- Ślusarczyk-Kacprzyk W, Skrzyński W, Fabiszewska E: Evaluation of doses and image quality in mammography with screen-film, CR, and DR detectors – application of the ACR phantom. Pol J Radiol, 2016; 81: 386–91
- Lewicki A, Jakubowski W: Instrumental basics of ultrasound imaging in grayscale. Part 2. Przegląd Urologiczny, 2014; 88(6): 6–17 [in Polish]
- 20. CIRS. General purpose multi-tissue ultrasound phantom, Model 040: User guide and technical information
- van Wijk MC, Thijssen JM: Performance testing of medical ultrasound equipment: fundamental vs. harmonic mode. Ultrasonics, 2002; 40(1-8): 585-91
- Thijssen JM, Weijers G, de Korte CL: Objective performance testing and quality assurance of medical ultrasound equipment. Ultrasound Med Biol, 2007; 33(3): 460–71
- Gibson NM, Dudley NJ, Griffith K: A computerised quality control testing system for B-mode ultrasound. Ultrasound Med Biol, 2001; 27(12): 1697–711